



Laboratoire national de métrologie et d'essais

Dr Jean-Rémy FILTZ



Thermal and Optical Properties of Materials

Recent Developments at LNE in the field of Energy

Natural Gas Development of a reference Calorimeter

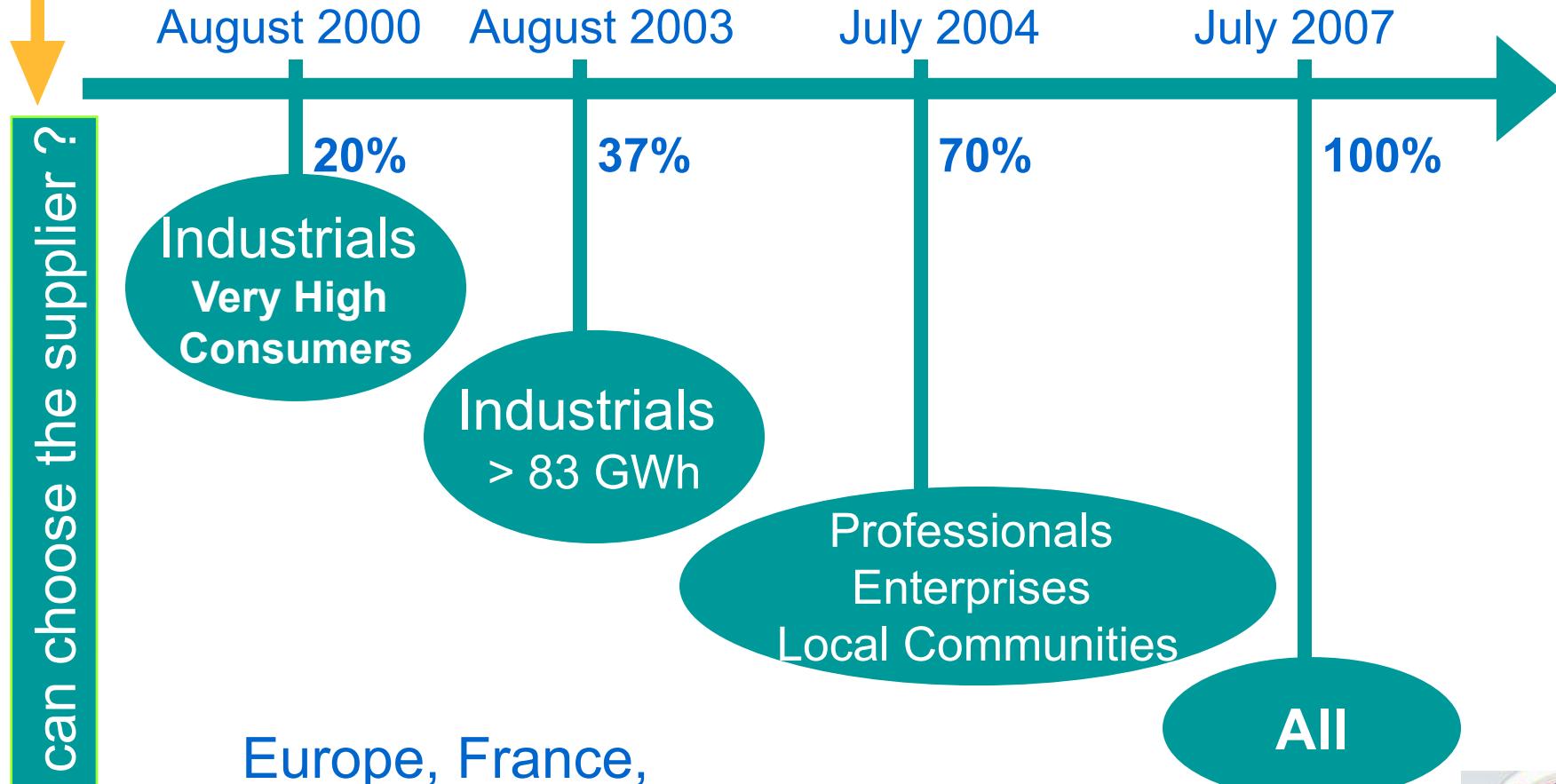
LNE expert: Dr Frédérique HALOUA



- Background and objectives
- Calorimeter principle
- Gross calorific value determination
- Modelling
- Calorimeter description - Details
- Experimental results - Perspectives
- Conclusions



Natural Gas Market; Key dates



Background



Today
2008



What does it mean in Europe and in France ?



Santiago de Querétaro,
México, 2008-10-24

- Opening of the natural gas market in Europe
 - Non constant natural gas composition flowing in the pipes
 - Accurate energy measurements * needed
- Improvement of the transported and distributed gas transactions by more accurate measurement of natural gas gross calorific value (GCV)

• GCV = Quantity of heat released by complete combustion of a specified gas quantity

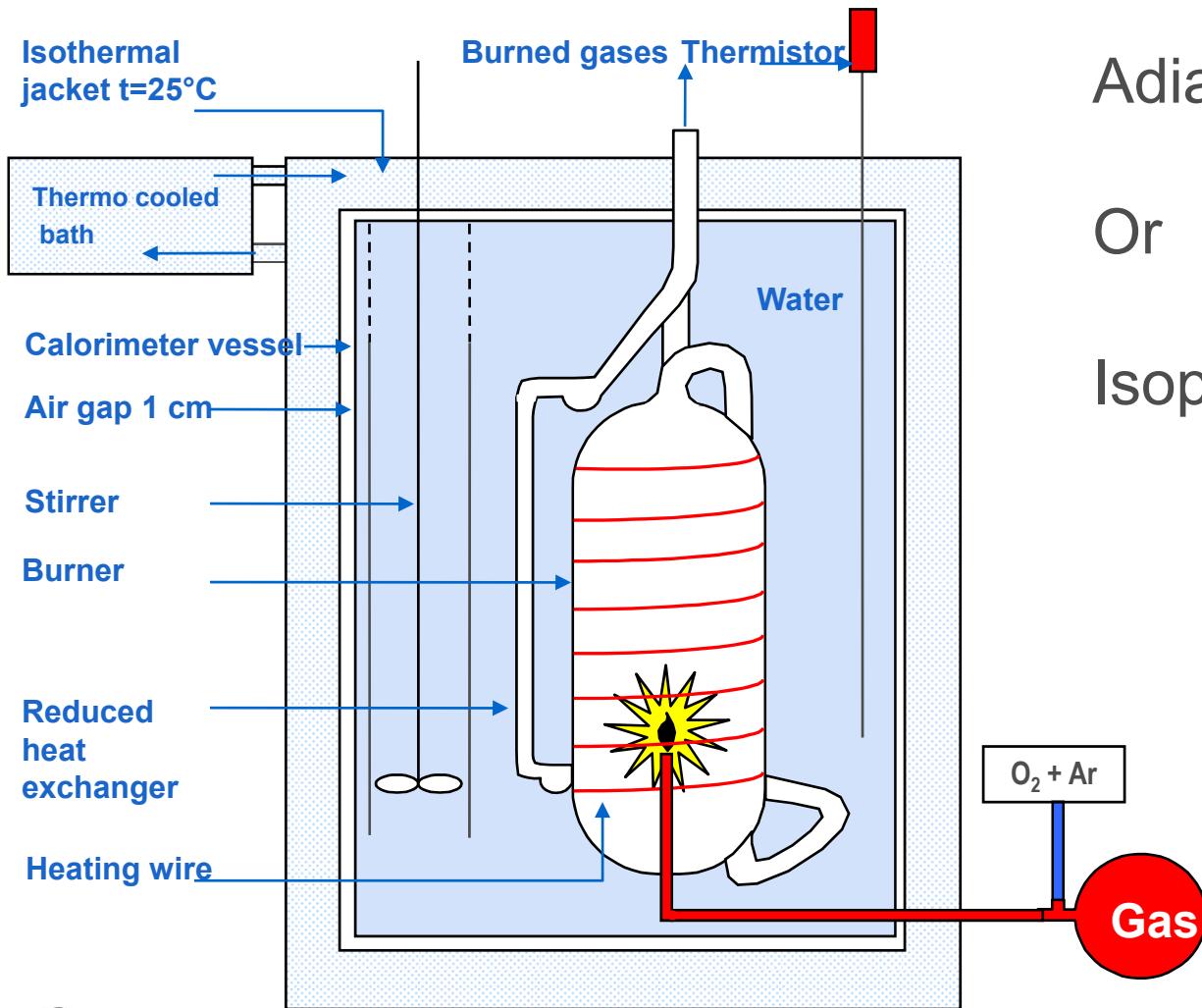


Thermal and Optical Properties of Materials
A Panorama of Key Recent Developments at LNE

- Redefinition of the values of the ISO 6976 standard
- Calibration of calorimeters and chromatographs
- Participation to the determination of energetic characteristics of sustainable energy products (natural gas, and also biofuels, biogases)
- Strengthening the metrological reference infrastructure in calorimetry in Europe (Germany, France, at least) and also in Russia, Ukraine...



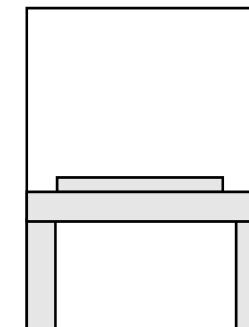
Calorimeter Principle



Adiabatic Calorimeter ?

Or

Isoperibolic Calorimeter ?

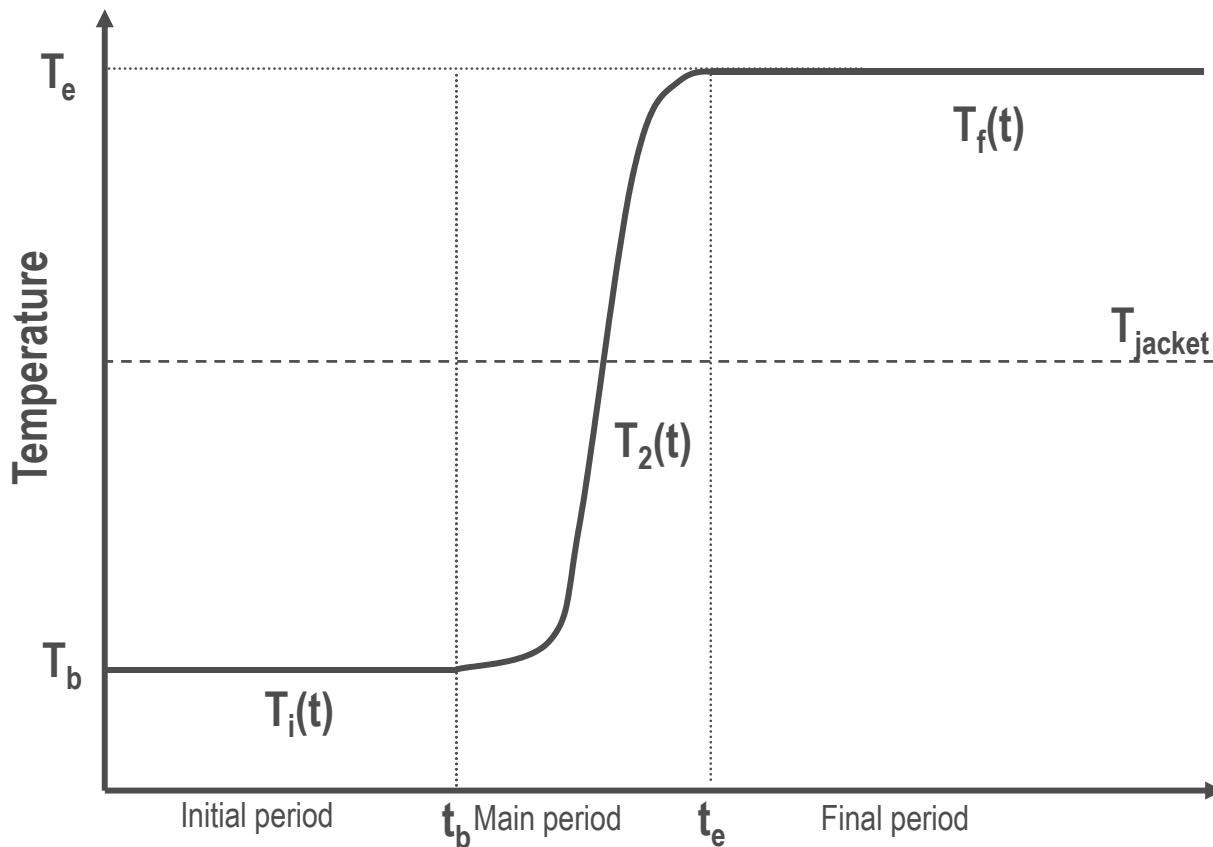


Mass comparator



Calorimeter Principle

Standard temperature curve of the water bath during heat release process



Adiabatic calorimeter

$$\Delta T_{ad} = T_e - T_b$$

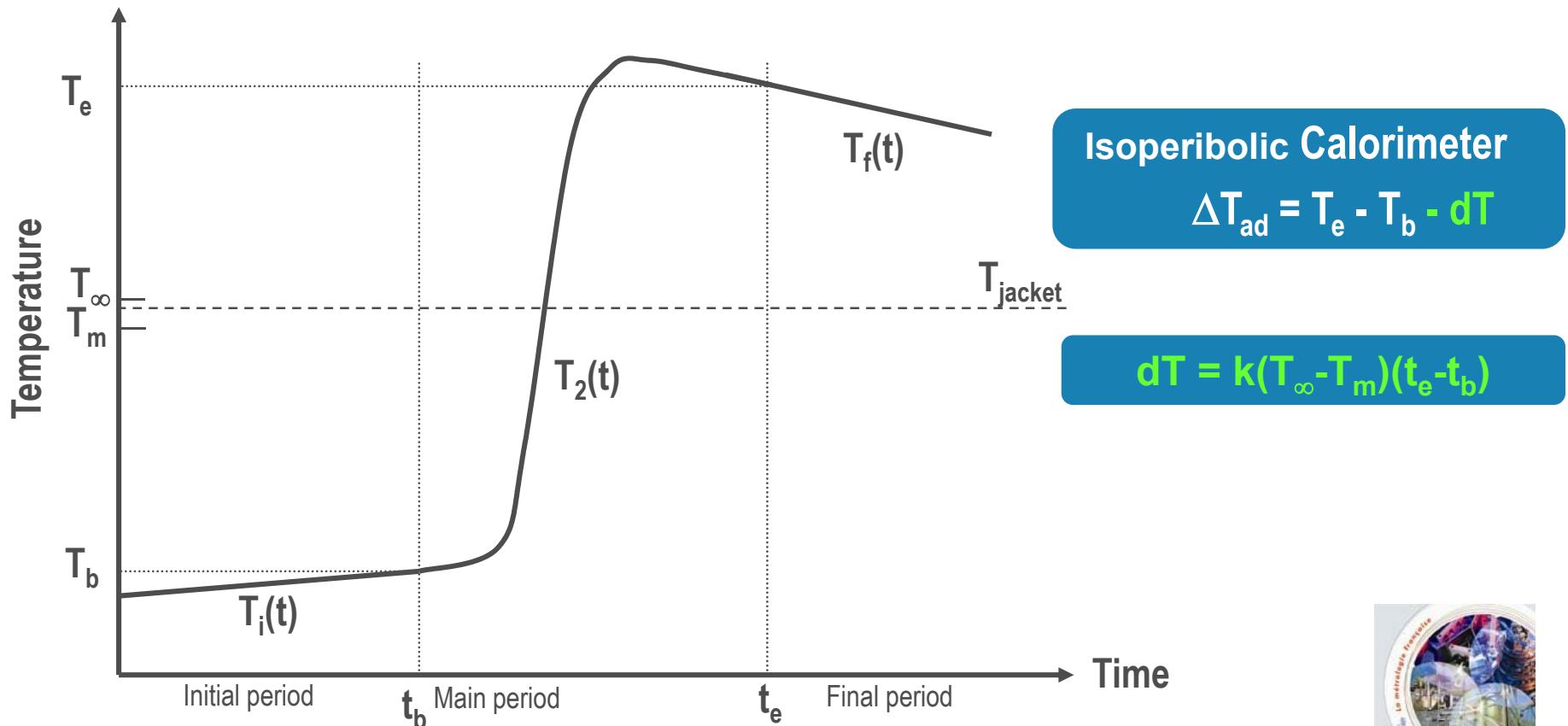
Three phases:

- initial period
- main or heat release period
- final period

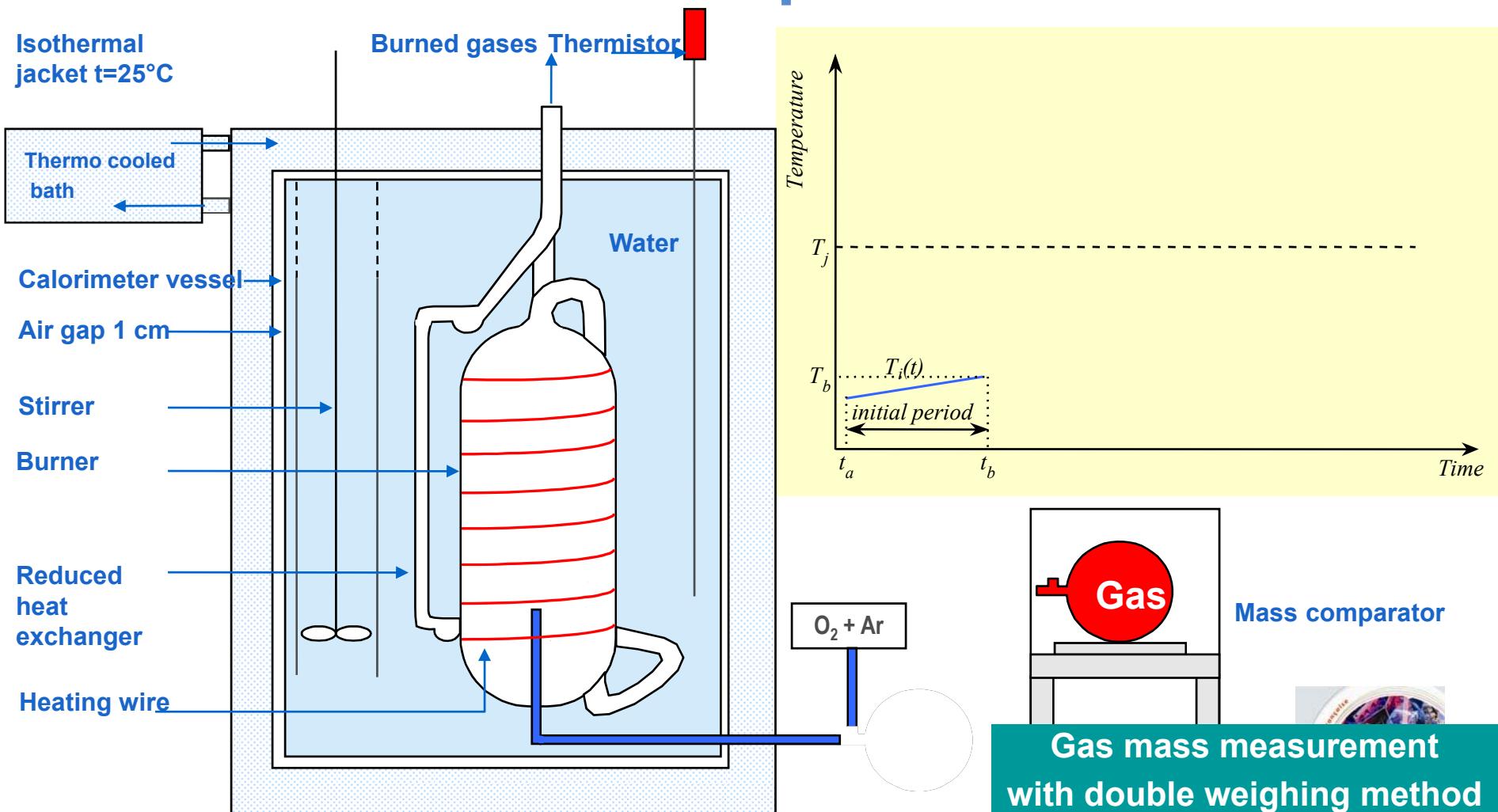


Calorimeter Principle

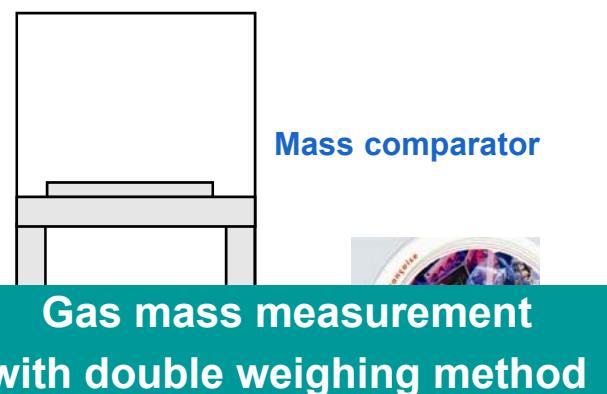
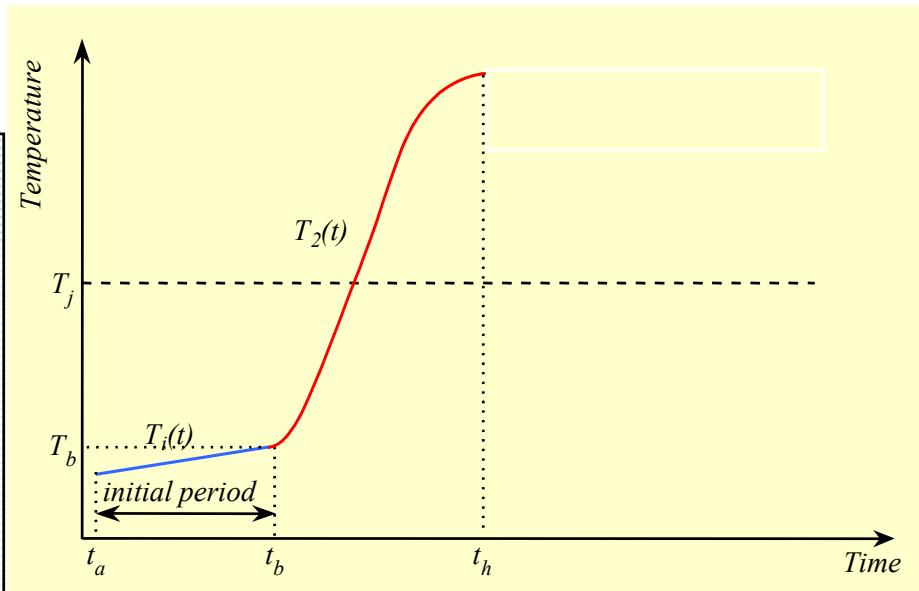
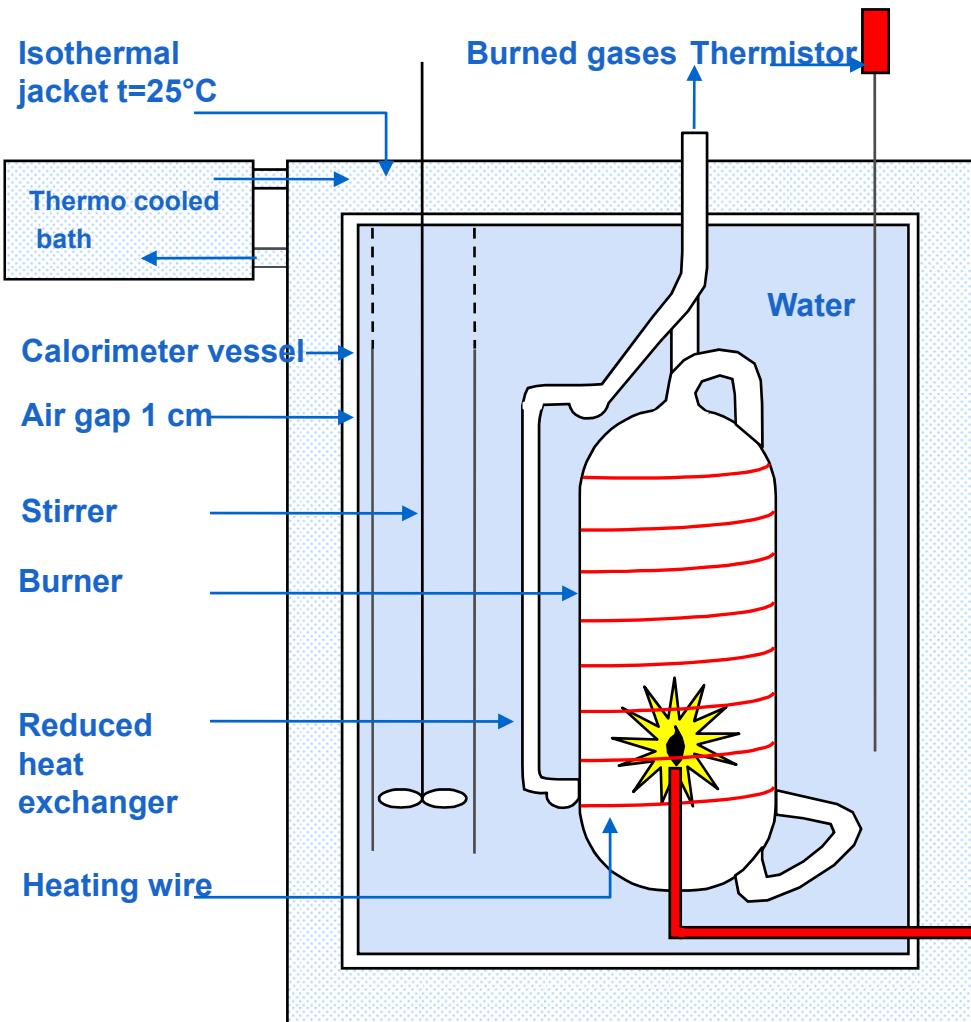
Standard temperature curve of the water bath
during heat release process



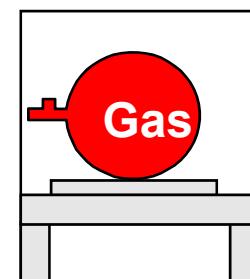
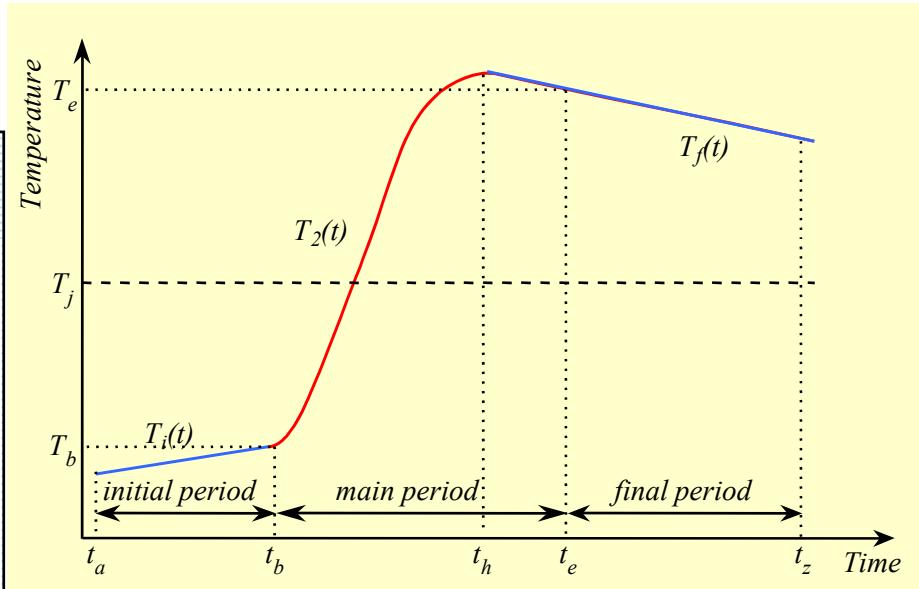
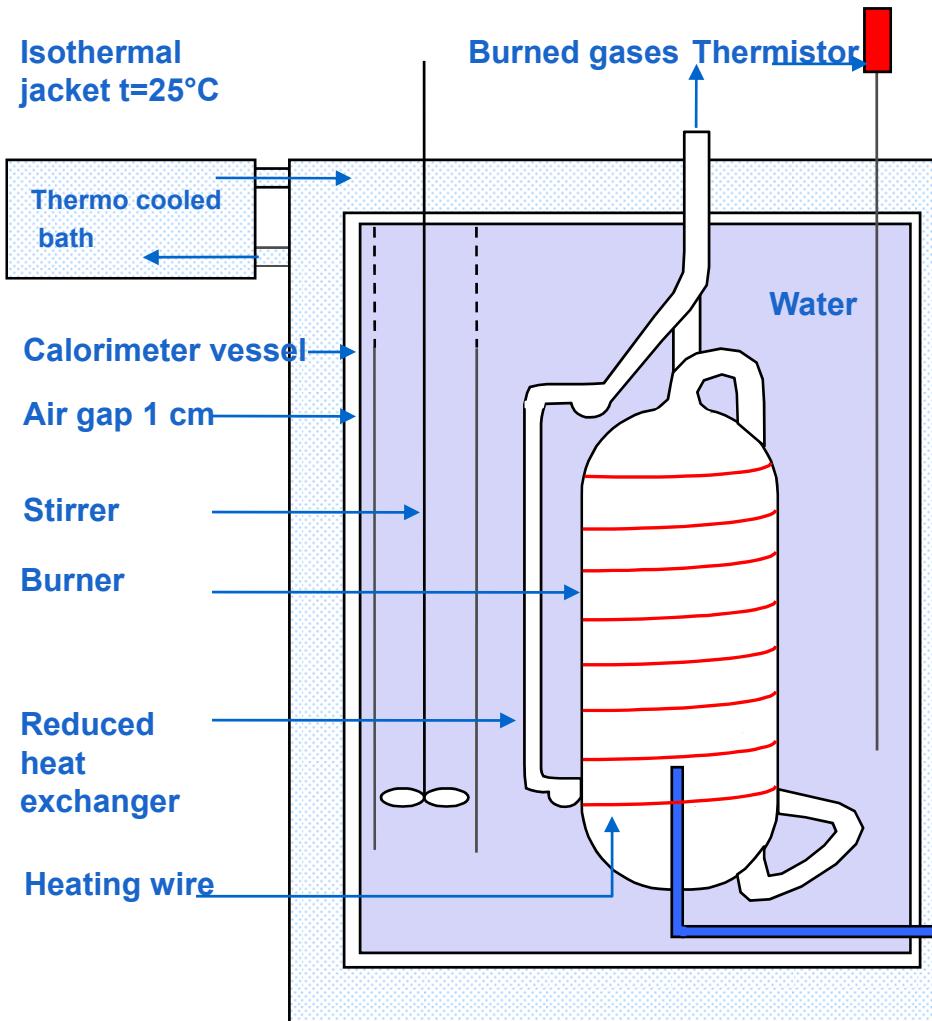
Principle



Principle



Principle

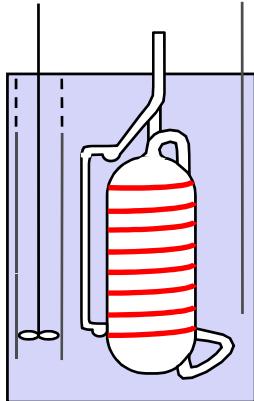


Gas mass measurement
with double weighing method



Gross Calorific Value determination

$$C_{cal} = \frac{\sum_i U_{heati} U_{refi} t_i}{R_{ref} \Delta T_{cal,ad}}$$



$$\Delta T_{comb,ad} = T_e - T_b - k(T_\infty - T_m)(t_e - t_b)$$

Depends on:

- temperature-time curve treatment

$$GCV = \frac{C_{cal} \Delta T_{comb,ad} + K}{m_{gas}}$$

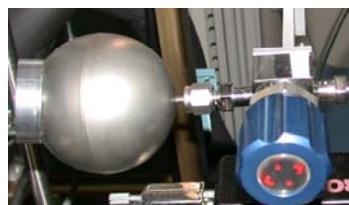
Depends on:

- heating wire voltage
- standard resistor (voltage and value)
- adiabatic temperature rise from calibration run

$$K = E_w + E_g - E_i$$

Depends on:

- electrical ignition energy E_i
- energy due to water leaving the calorimeter during the experiment E_w
- energy traducing the difference of the in and out flowing gases temperatures E_g



$$m_{gas} = M_{post-comb} - M_{fore-comb}$$

Depends on:

- calibrated masses,
- density (air and calibrated masses)
- volume of calibrated masses

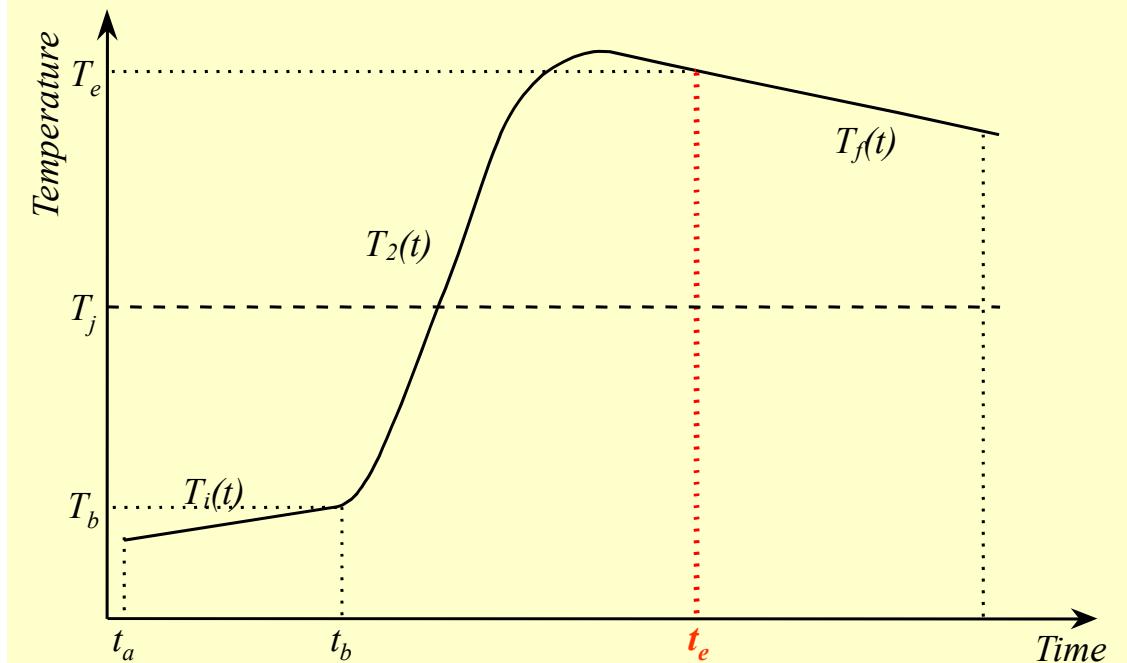


General equation

$$\Delta T_{comb,ad} = T_e - T_b - k(T_\infty - T_m)(t_e - t_b)$$

Chronological calculation steps for the determination of ΔT_{ad}

- Determination of t_e



General equation

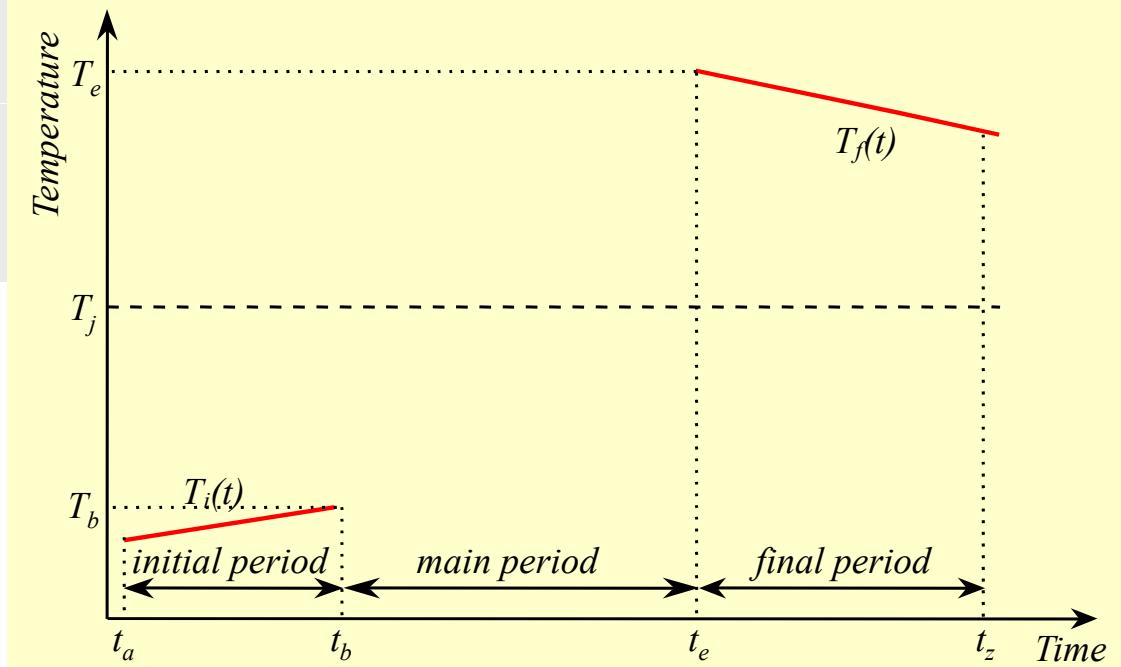
$$\Delta T_{comb,ad} = T_e - T_b - k(T_\infty - T_m)(t_e - t_b)$$

Chronological calculation steps for the determination of ΔT_{ad}

- Determination of t_e
- Exponential simultaneous regression of the initial and final periods

$$T(t) = T_\infty - [T_\infty - ((1-y)T_b + yT_e)] \exp(-k\tau)$$

Calculation of T_e , T_b , k and T_∞



General equation

$$\Delta T_{comb,ad} = T_e - T_b - k(T_\infty - T_m)(t_e - t_b)$$

Chronological calculation steps for the determination of ΔT_{ad}

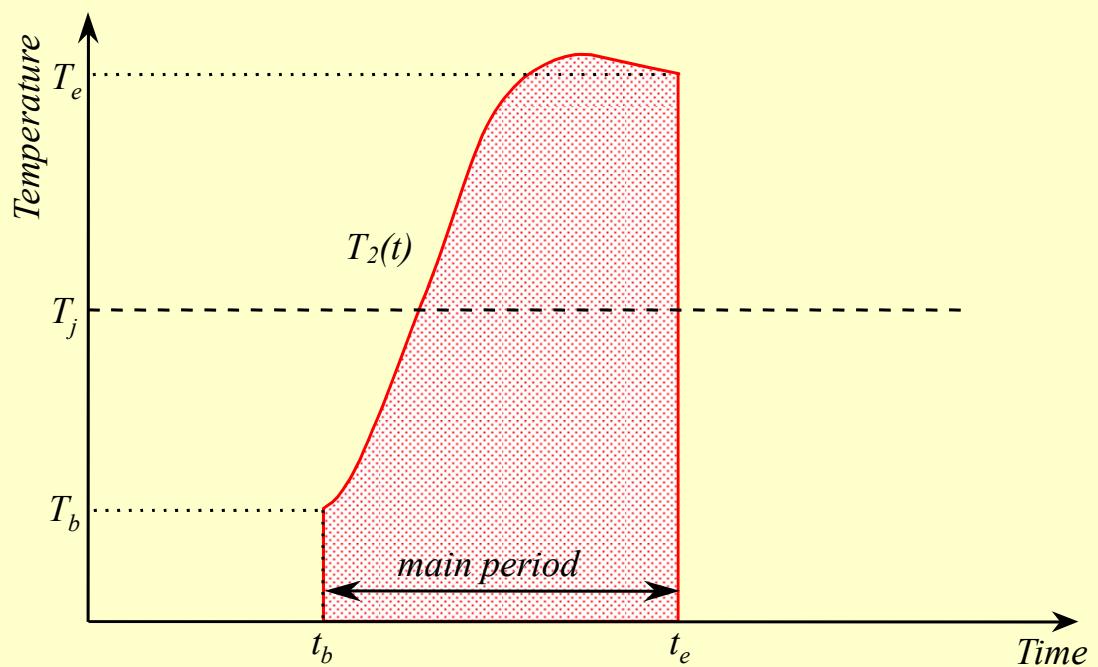
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Calculation of T_e , T_b , k and T_∞

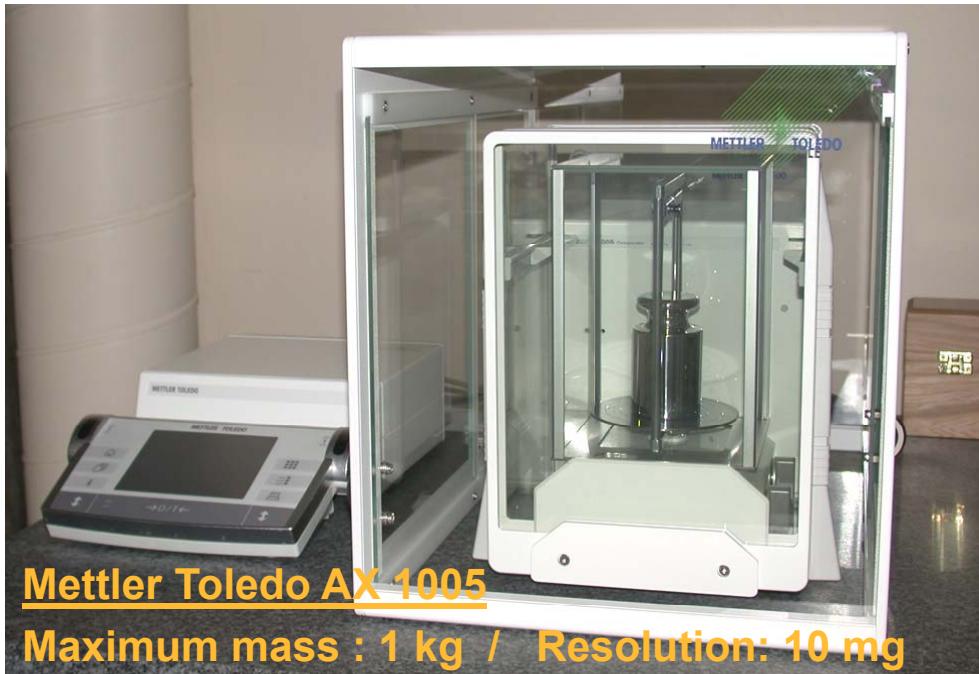
- Calculation of $T_m = \frac{1}{t_e - t_b} \int_{t_b}^{t_e} T_2(t) dt$ by the trapezoidal method

- Calculation of $dT = k(T_\infty - T_m)(t_e - t_b)$
- Calculation of $\Delta T_{ad} = T_e - T_b - dT$

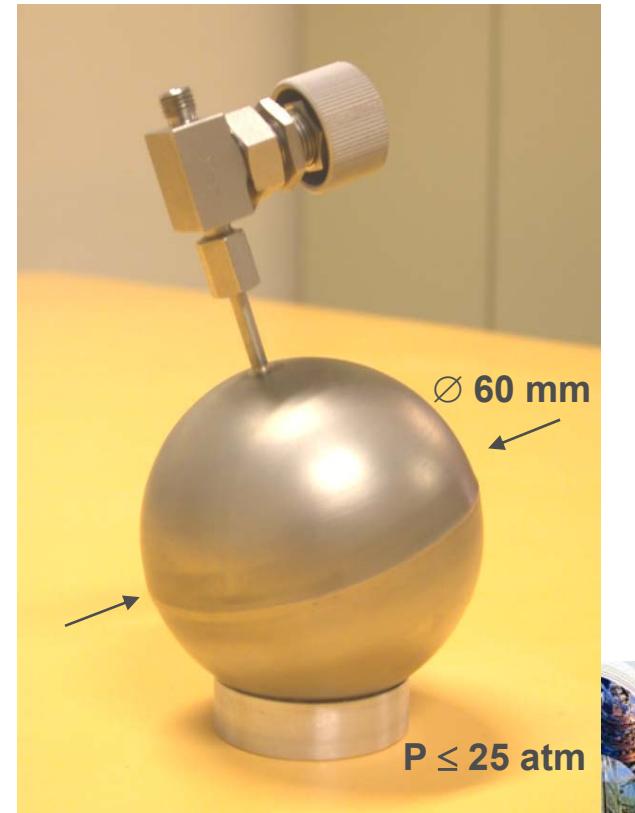


Gas weighing system

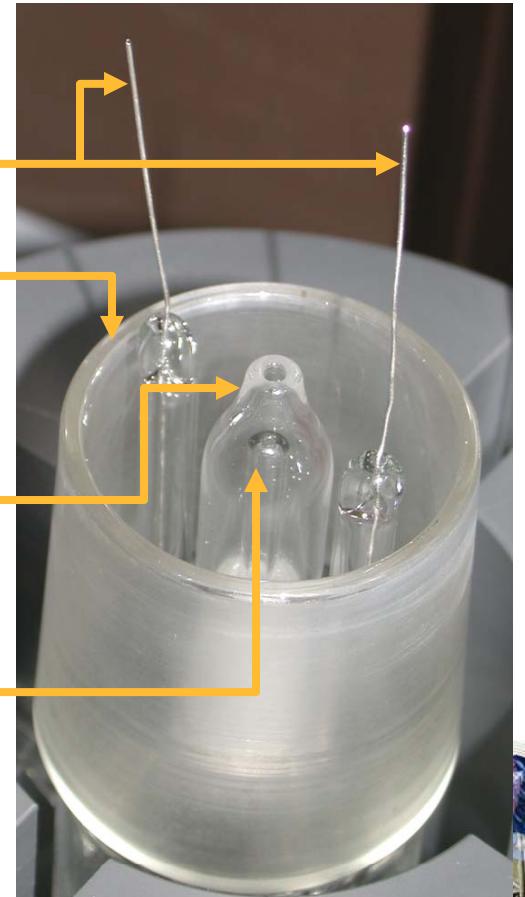
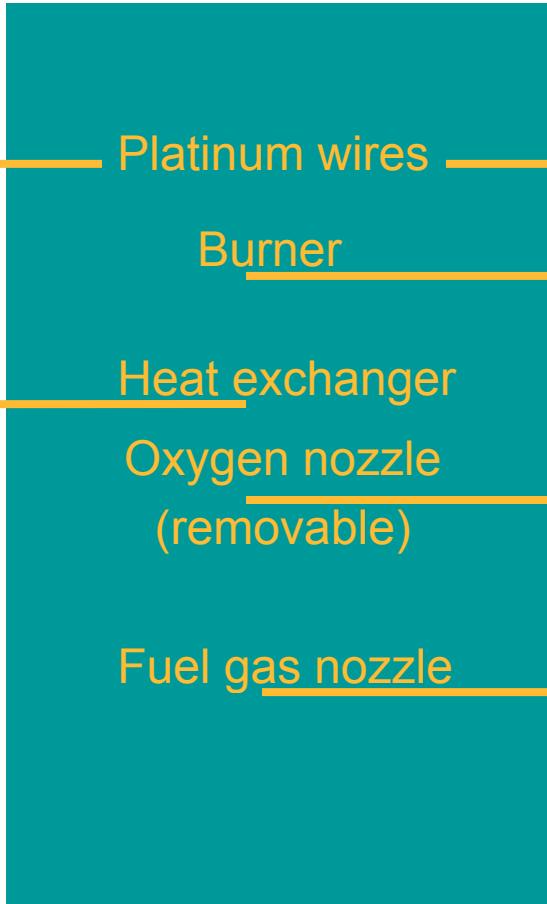
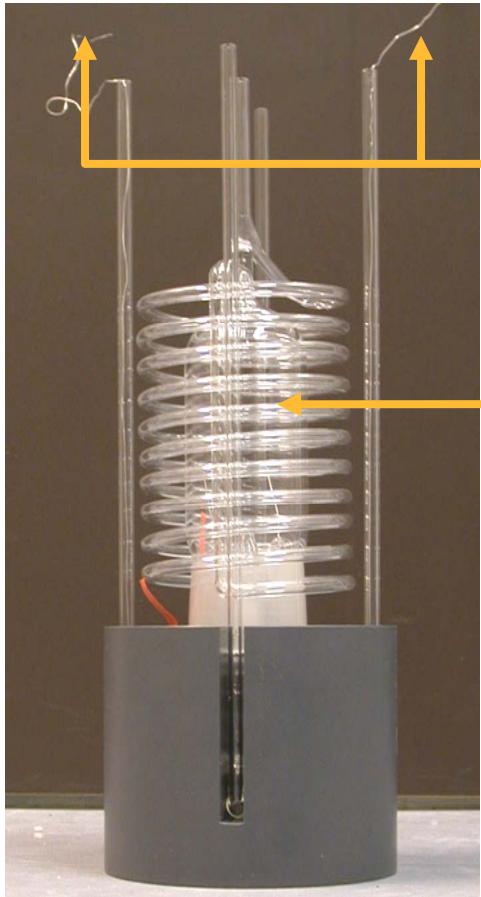
Mass comparator



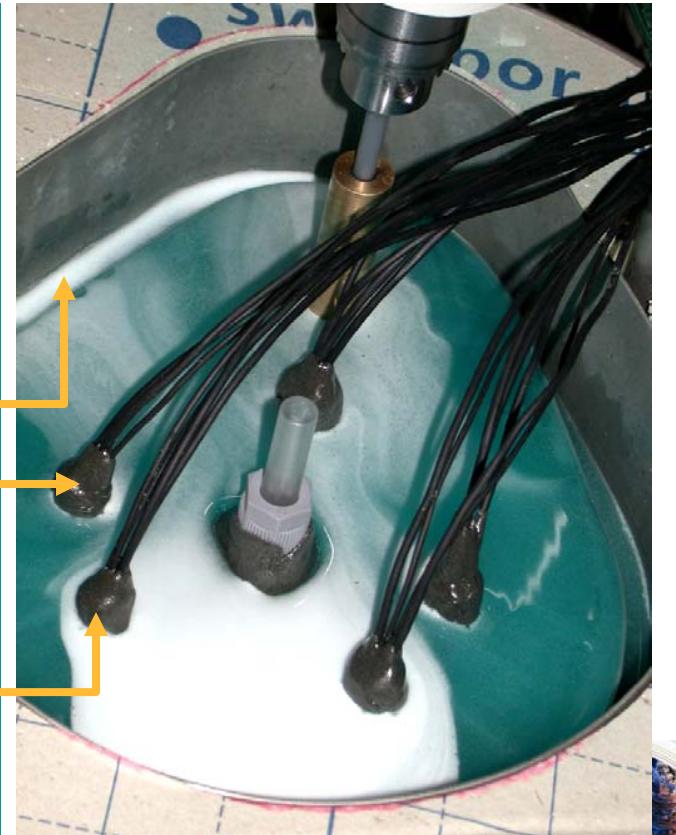
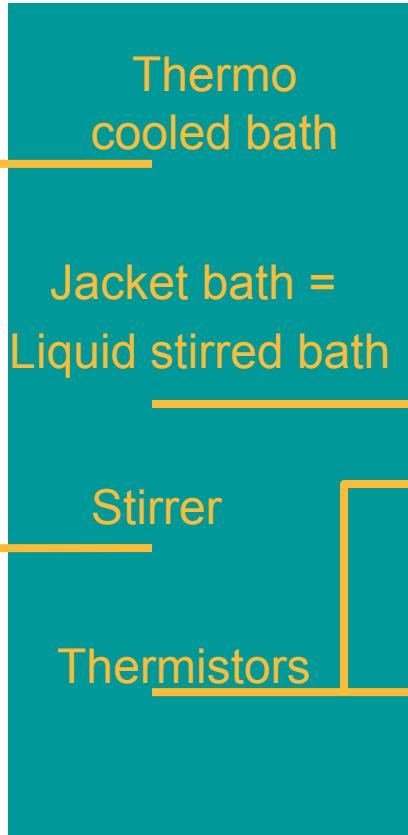
Sphere



Combustion Chamber and Burner



Calorimetric Vessels

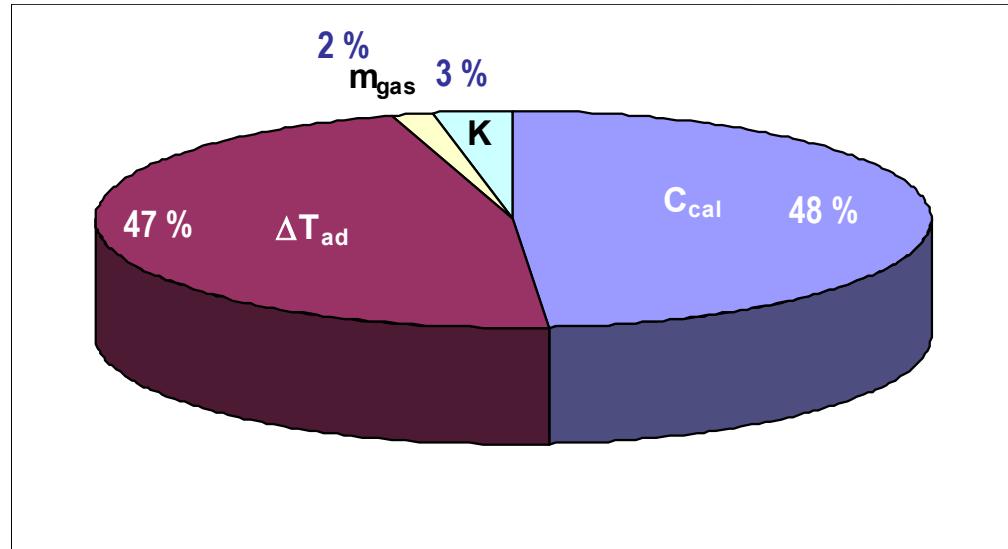


Uncertainty contributions

$$GCV = \frac{C_{cal} \cdot \Delta T_{ad} + K}{m_{gas}}$$



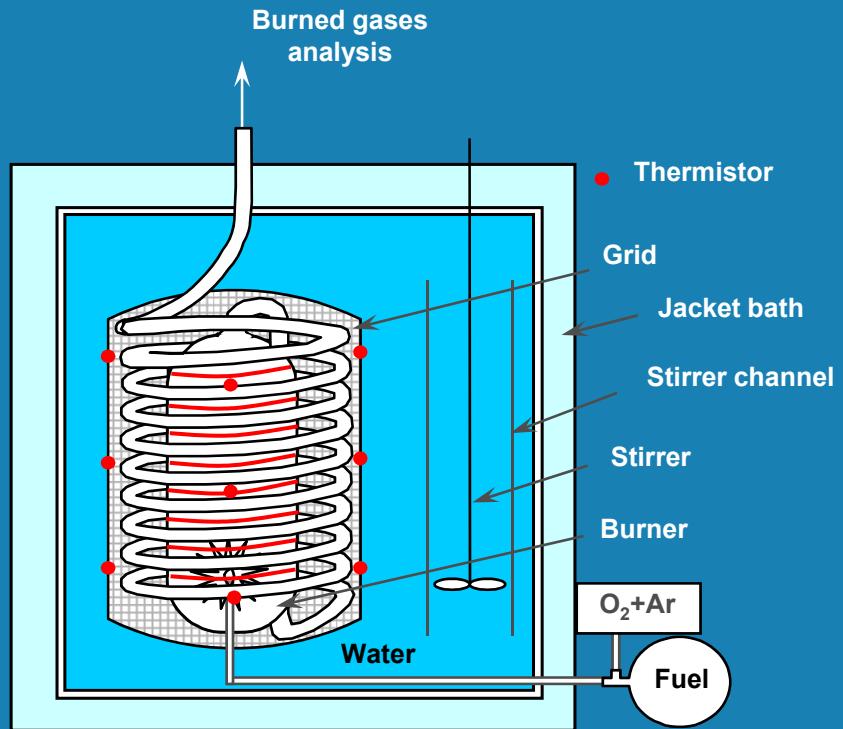
$$U(GCV) \leq 0,05\%$$



- ✓ C_{cal} : heat capacity of the calorimeter
- ✓ ΔT_{ad} : adiabatic temperature rise
- ✓ K : energetic correction factor
- ✓ m_{gas} : mass of fuel gas



Experimental data obtained by electrical dissipation



- Electrical energy dissipation in the bath during 20 minutes with a heating coil located around the burner
- Temperature rise measurements with 9 thermistors immersed in the water bath

Thermistors characteristics

- Sensitivity: 430 W/°C
- Small geometry: glass bead probes of $\sim \varnothing 1$ mm
- Fast response time: 1.5 sec in an oil stirred bath

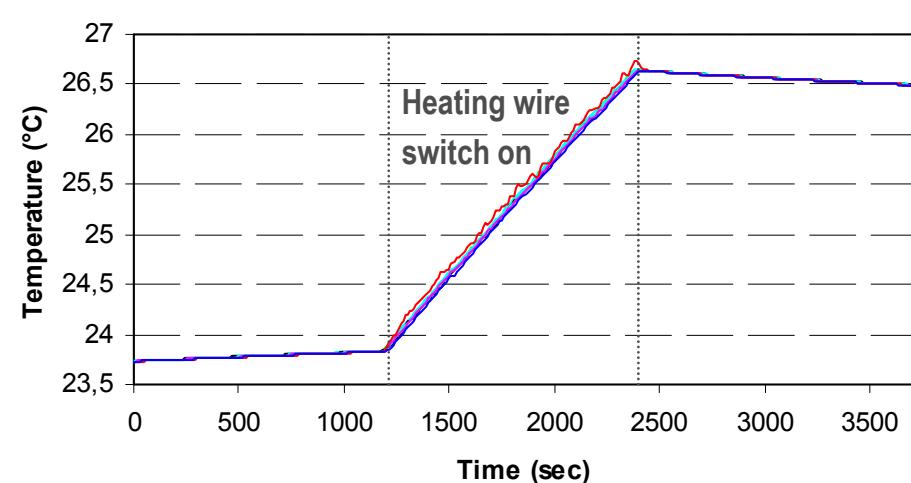


Preliminary measurements

Experimental data obtained by electrical dissipation

Input parameters:

- $T_{jacket} = 25^\circ\text{C}$
- Stirrer speed = 600 rpm
 - Water velocity in the outflow of the stirrer channel: 30 cm/s
- $P_{stirrer} : 0,39 \text{ W}$
- $P_{heater} = 50 \text{ W}$



Experimental temperature rise	2.7713 K	Each period: 20 minutes
Standard deviation due to non homogeneity in the water bath	1.4 mK in the stable periods (initial and final periods)	
	32.3 mK in the dynamic regime (heat release period)	

Input parameters have been optimised operating a modelling

Thermal heat transfer modelling in the calorimeter

- Inventory of all the heat transfer types in the calorimeter
 - Importance of heat transfer by radiation
- Quantitative estimate of these heat transfers given by:
 - Mass and geometry (thickness, ρ , m)
 - Materials (λ , C_p , ε)
 - Temperature levels and total released power
 - Observed water flow in the bath



Overall validation of the numerical model

- Overall validation of the numerical model under the following conditions:
 - ✓ Maximal heat transfer from the burner to the water bath
 - ✓ Minimal heat loss to the jacket
- Recommendation for the 3D simulation implementation
 - ✓ to measure the water speed at the exit of the stirrer channel to identify the water flow regime: laminar or turbulent
 - ✓ to consider as stagnant the air between the inner and the outer vessels
 - ✓ to activate a radiative numerical model for combustion tests

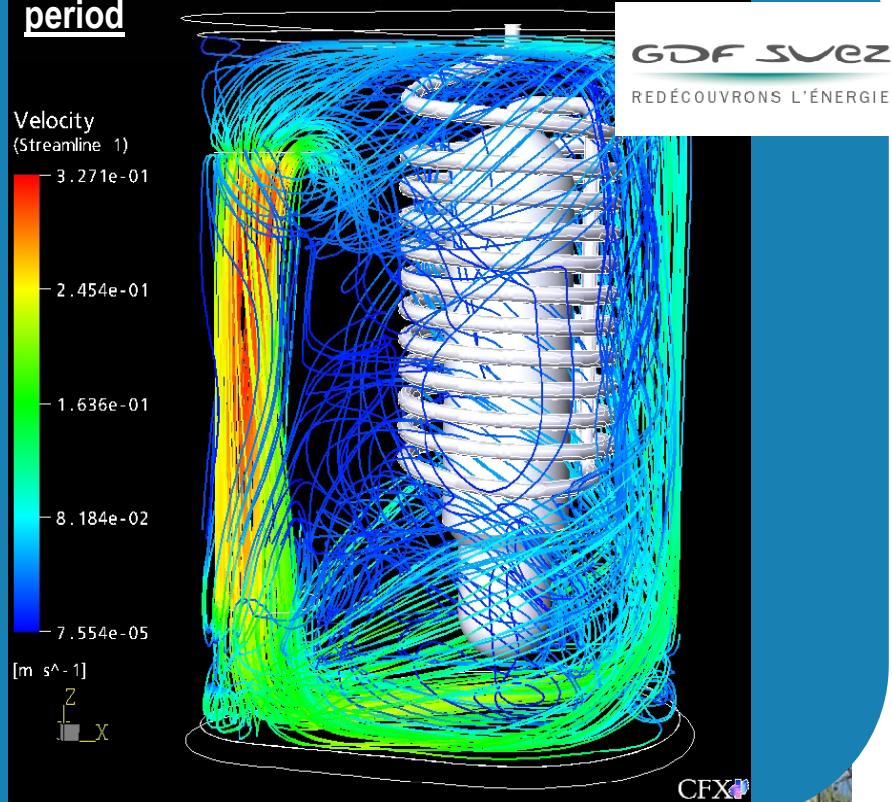
CFD 3D numerical model

Input parameters:

- No heating
- Water velocity in the outflow of the stirrer channel: 30 cm/s
- P_{stirrer} : 0,39 W
- T_{jacket} : 27 °C
- $T_{\text{calorimeter bath}}$: 22 °C

Large exterior circulation loop creates almost stagnant regions between:
• burner and heat exchanger coil
• stirrer channel and burner

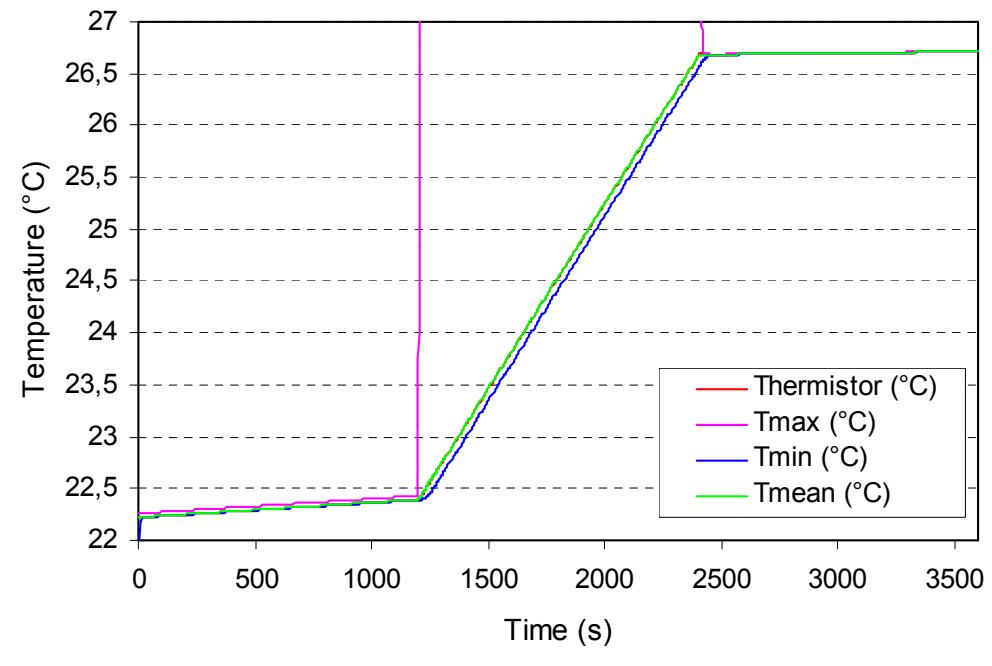
Stream lines of the water flow in the initial period



CFD 3D numerical model: Electrical dissipation

Input parameters:

- Convective heat flux applied uniformly over 10 cm height on the burner
- No heat transfer by radiation
- Water velocity in the outflow of the stirrer channel: 30 cm/s
- P_{stirrer} : 0,39 W
- T_{jacket} : 27 °C
- P_{heater} : approx. 60 W

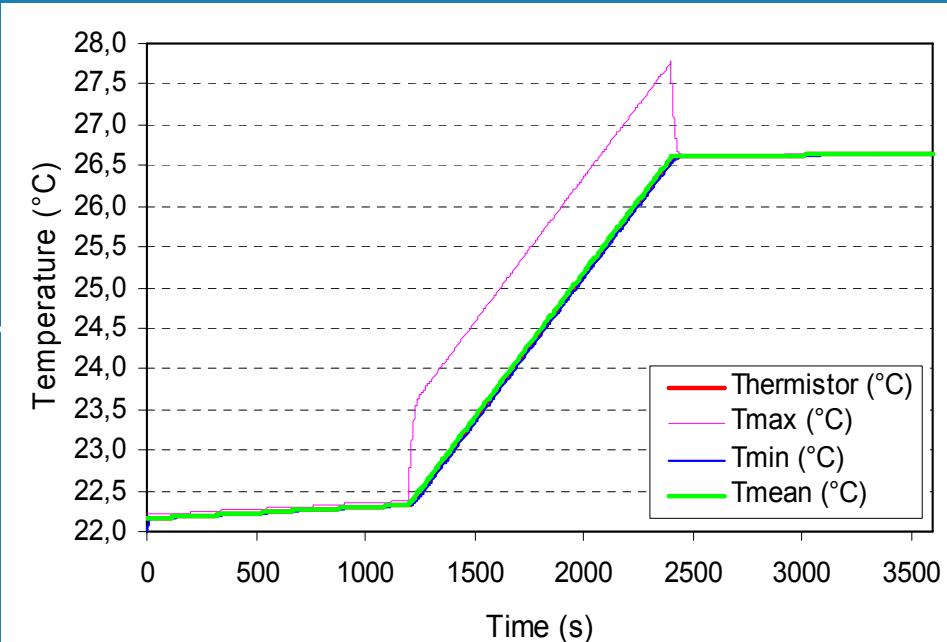


- Good homogeneity in the bath during the power release
- Validation of thermistor location

CFD 3D numerical model: Combustion heating

Input parameters:

- Pure radiative heat flux applied uniformly over 10 cm height on the burner
- Water velocity in the outflow of the stirrer channel: 30 cm/s
- P_{stirrer} : 0,39 W
- T_{jacket} : 27 °C
- P_{heater} : approx. 60 W



- Same general thermal behaviour as in the convective heat flux
- Validation of thermistor location
- The only difference concerns maximum temperature evolution

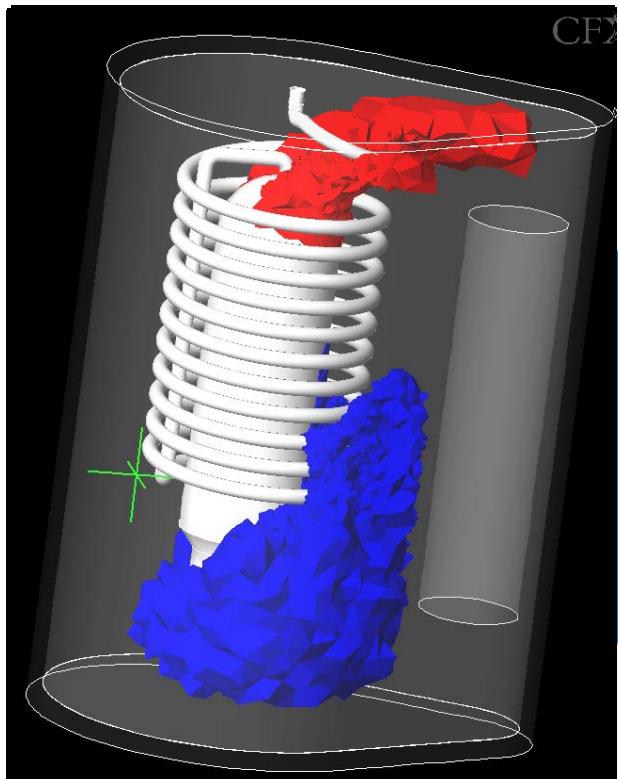
Comparison of the two theoretical heating cases

	$T_{max} - T_{mean}$ (K)	$T_{mean} - T_{min}$ (K)
Pure convective heating	1.17	8.54
Pure radiative heating	0.08	0.13



CFD 3D numerical model

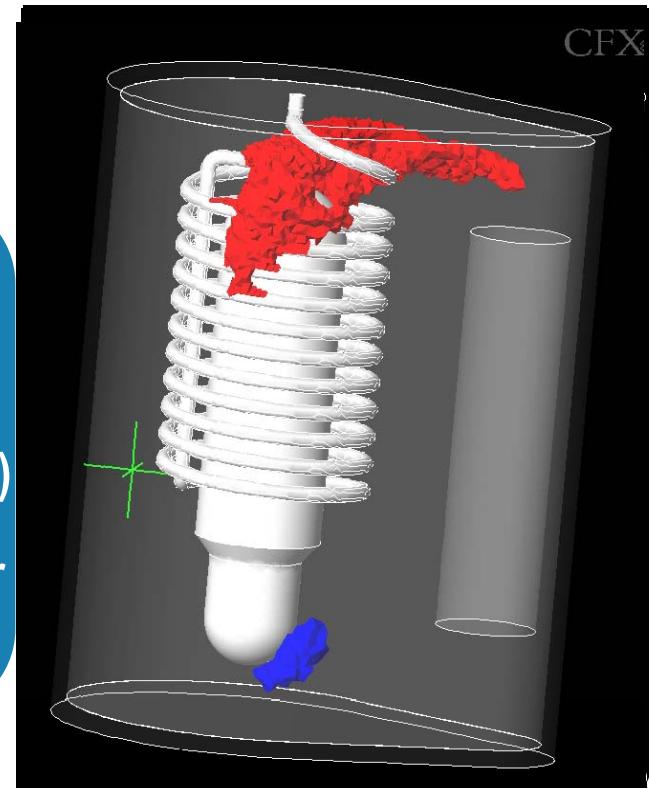
Temperature evolution in the bath during heat release



Convective power release
(electrical calibration)

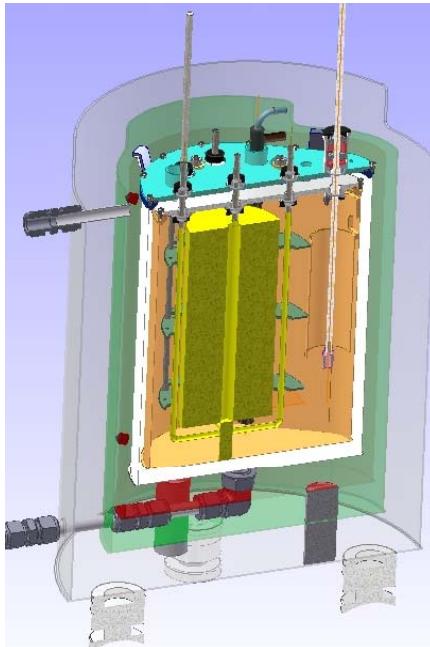
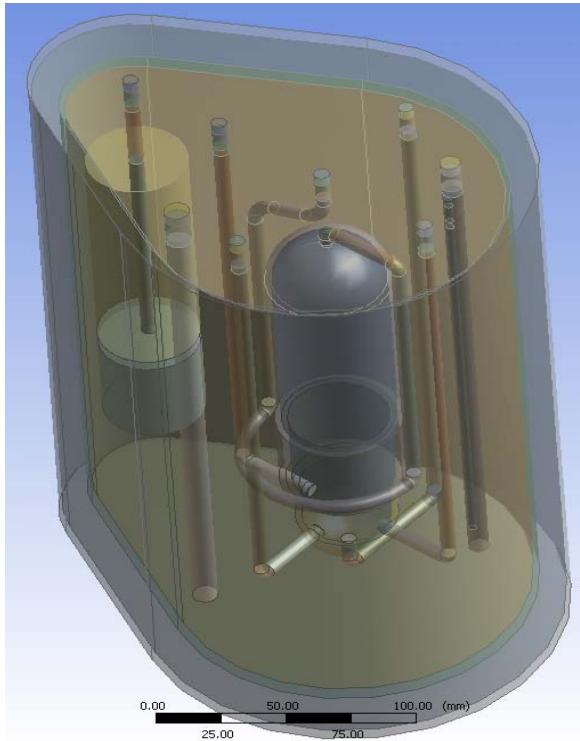
$t = 2410 \text{ s}$

Volume of water where
 $T \geq T_{\text{mean}} + 50 \text{ mK}$ (in red)
 $T \leq T_{\text{mean}} - 50 \text{ mK}$ (in blue)
The location of the thermistor probe is critical



Radiative power release

Modelling, Dimensioning the device



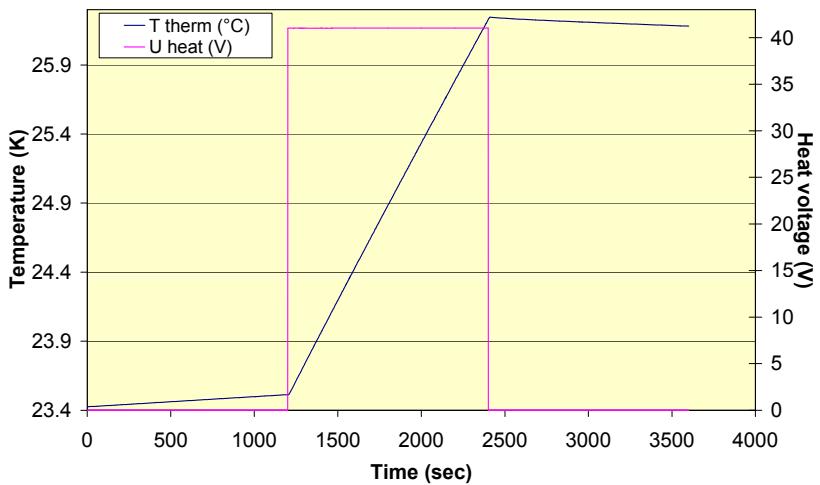
- **Realization of the final version of the calorimeter**
 - New internal and external electro polished vessels
 - Modification of the tightness system of the vessels
 - Implementation of an optical flame detector



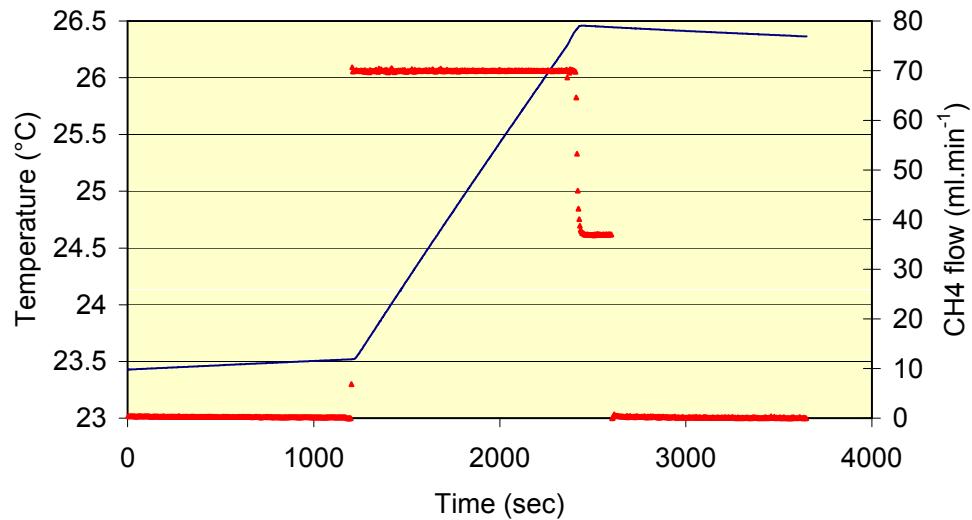
Experimental results

Two experiments → One GCV calculation

Calibration



Combustion



$$\Delta T_{cal,ad} = T_e - T_b - k(T_\infty - T_m)(t_e - t_b)$$

$$\Delta T_{comb,ad} = T_e - T_b - k(T_\infty - T_m)(t_e - t_b)$$

$$C_{cal} = \frac{\sum_i U_{heat,i} U_{ref,i} t_i}{R_{ref} \Delta T_{cal,ad}}$$

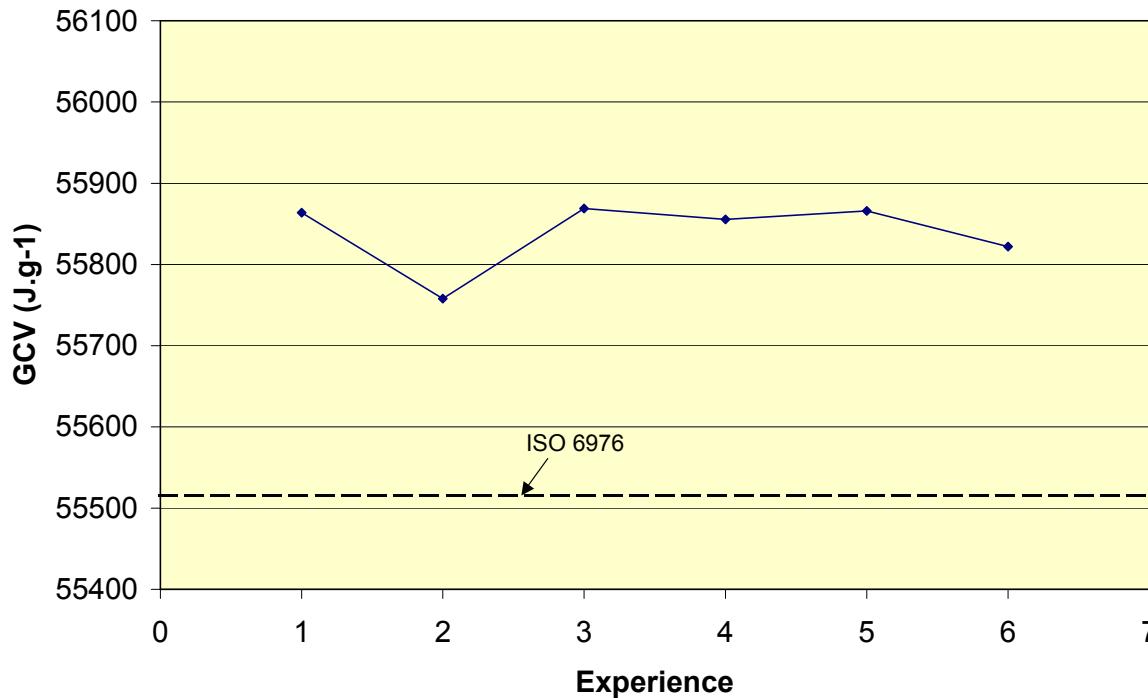
$$GCV = \frac{C_{cal} \Delta T_{comb,ad} + K}{m_{gas}}$$

Santiago de Querétaro,
México, 2008-10-24

Thermal and Optical Properties of Materials
A Panorama of Key Recent Developments at LNE



Experimental results, Perspectives



Repeatability measurements of GCV with the prototype version of the calorimeter

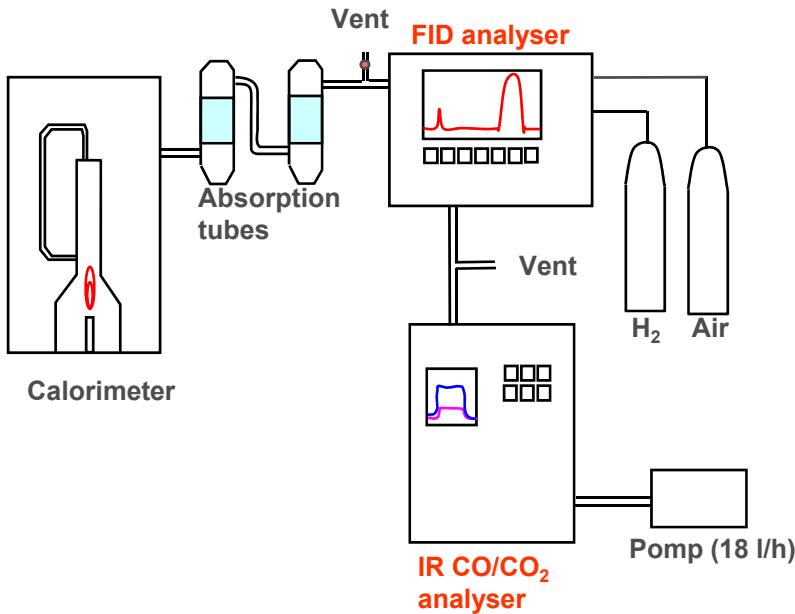
On 6 experiments

- Mean value = 55839 J.g⁻¹
- Standard deviation = 0.077 % (0.16% on 11 experiments)
- Relative deviation between the experimental mean and normalised value given by ISO 6976 of 0.58 %

- Reduction of unburned methane quantity
- Implementation of a non-calibrated hydrocarbon analyser (FID method)



Unburned methane analysis



Implementation of a non-calibrated hydrocarbon analyser (FID method) in series with an infra-red CO / CO₂ analyser

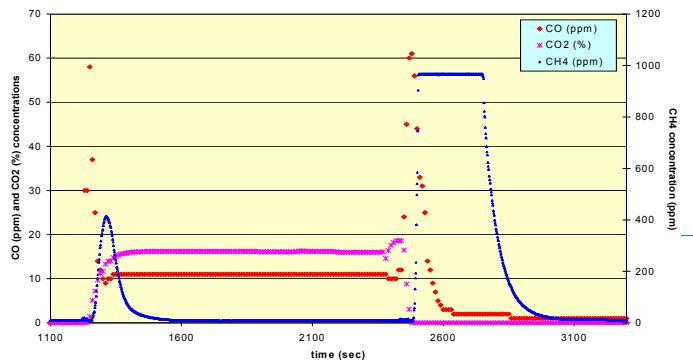
Continuous measurements of CH₄ concentration



Unburned methane analysis

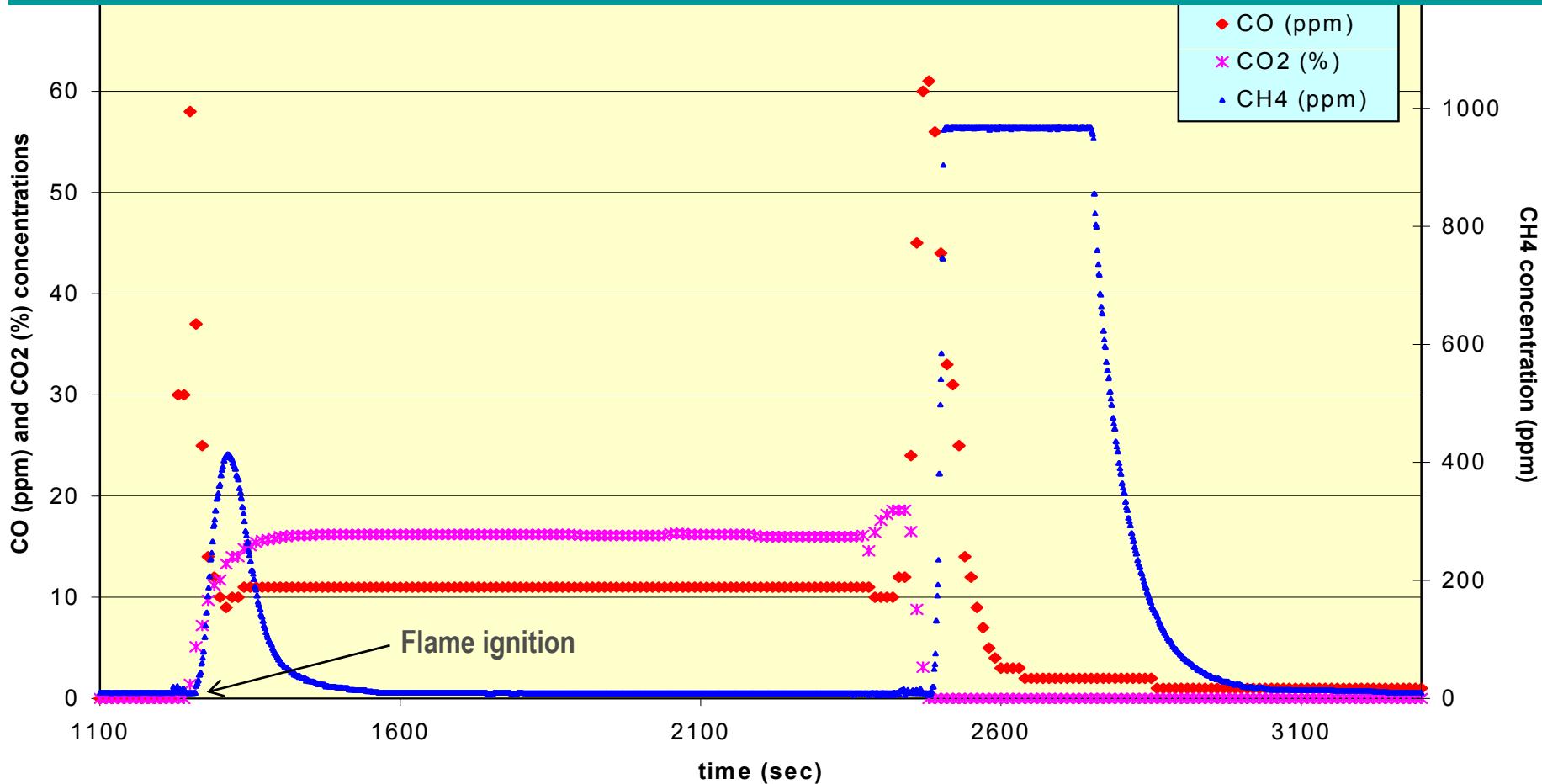
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Continuous measurements of CH₄ concentration



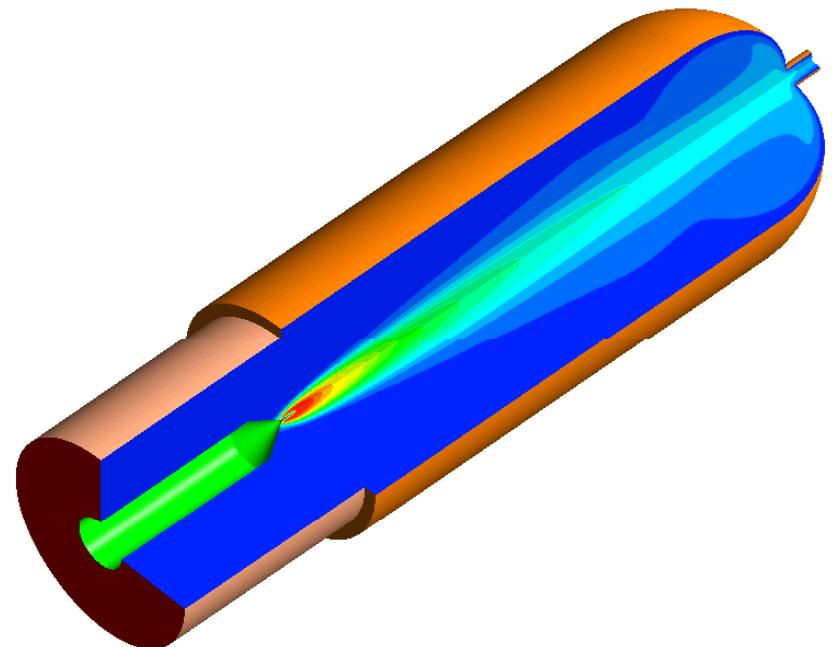
- Total combustion (*except at ignition and extinction periods*)
- Bad combustion at flame ignition and extinction
 - ⇒ non-ideal mixture CH₄/O₂ and unstable inflow gases
- Time delay between CH₄ and CO picks
 - ⇒ different analyser times response (FID and IR)
- Maximum CH₄ at flame extinction (saturation), lower at ignition

Unburned methane analysis



Improvement axes

- Flushing the methane pipes with Argon to help combustion at the end of the experiment
- Implementation of a chemical catalyser in the burner or in the heat exchanger to help combustion of the remaining methane
- Correct the GCV value by calculating the unburned methane concentration with the FID analyser



- Detailed calculation of the gross calorific value with a reference calorimeter
- First repeatability study
- Numerical simulations → optimised design geometry (burner, vessels, stirrer, location of the temperature sensor, ...)
- Measurements with the improved calorimeter
- Measurement of homogeneity uncertainty of the water bath
- Inter-comparison with national metrology institutes on GCV of methane (CCT WG9)
- Application for biofuels ?



LNE, Sponsors and Partners

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- Institut de Radioprotection et de Sûreté Nucléaire (IRSN)
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Thank you for your Attention

Gracias por su atención

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